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Nuclear

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Dresden Nuclear Power Station, Unit 3 Facility Operating License No. DPR-25

NRC Docket No. 50-249

Subject:

Core Operating Limits Report for Unit 3 Cycle 18

The purpose of this letter is to transmit the Core Operating Limits Report (COLR) for the upcoming operating cycle (D3C18) in accordance with Technical Specification (TS) Section 5.6.5, "CORE OPERATING LIMITS REPORT (COLR)." The analytical methods used to determine the operating limits were NRC approved. The COLR is enclosed as an attachment to this letter

Should you have any questions concerning this letter, please contact Mr. J. Hansen at (815) 416-2800.

Respectfully,

R.J. Hovey

Site Vice President

Dresden Nuclear Power Station

Attachment: Core Operating Limits Report, Dresden Station Unit 3 Cycle 18, Revision 0

CC:

Regional Administrator – NRC Region III

NRC Senior Resident Inspector - Dresden Nuclear Power Station

DO01

Core Operating Limits Report

for

Dresden Unit 3 Cycle 18

Issuance of Changes Summary

Affected Section	Affected Pages	Summary of Changes	Revision	Date
All	All	Original Issue (Cycle 18)	0	10/02

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References

- 1. Exelon Generation Company, LLC Docket No. 50-249, Dresden Nuclear Power Station, Unit 3 Facility Operating License, License No. DPR-25.
- Letter from D. M. Crutchfield to All Power Reactor Licensees and Applicants, Generic Letter 88-16; Concerning the Removal of Cycle-Specific Parameter Limits from Tech Specs, October 3, 1988.
- 3. "Supplemental Reload Licensing Report for DRESDEN UNIT 3 Reload 17 Cycle 18", 0000-0006-9848-SRLR, Revision 1, August 2002.
- 4. "Determination of D3C18 MICROBURN GE14 LHGR Limits", BNDD:02-001, Revision 1, June 18, 2002.
- 5. "DRESDEN 2 and 3 QUAD CITIES.1 and 2 Equipment Out-Of-Service and Legacy Fuel Transient Analysis", GE-NE-J11-03912-00-01-R1, TODI NFM0100091 Sequence 01, November 2001.
- 6. "Instrument Setpoint Calculation Nuclear Instrumentation Rod Block Monitor Dresden 2 & 3", GE DRF C51-00217-01, December 15, 1999.
- 7. "OPL-3 Parameters for Dresden Unit 3 Cycle 18 Transient Analysis", TODI NF2002-9994, April 5, 2002.
- 8. "Fuel Mechanical Design Report Exposure Extension for ATRIUM-9B Fuel Assemblies at Dresden, Quad Cities, and LaSalle Units", EMF-2563(P) Revision 1, TODI NFM0100107 Sequence 0, August 2001.
- 9. "Determination of Generic MCPR_F Limits", BNDG:02-001, May 17, 2002.
- 10. General Electric Standard Application for Reactor Fuel (GESTAR II) and US supplement, NEDE-24011-P-A-14, June 2000.
- 11. Letter from Carlos de la Hoz to Doug Wise and Alex Misak, "Approval of GE Evaluation of MSIV out of Service for Dresden and Quad Cities", NFM-MW:02-0274, dated August 2, 2002.
- 12. "Dresden Unit 3 Cycle 18 FRED Form Revision 2", TODI NFM0200041 Sequence 02, April 24, 2002.
- 13. Letter from Russell Lindquist (GNF) to Jim Nevling (Exelon), "NFM-MW-B088 D3C18 Licensing Applicability Review", FRL02DR3-007, dated August 26, 2002.
- Letter from Anthony Giancatarino (Nuclear Fuels) to Doug Wise (Dresden), "Determination of Dresden Unit 3 Cycle 18 Middle of Cycle Exposure Point", NF-MW:02-0383, dated September 27, 2002.

1. Average Planar Linear Heat Generation Rate

1.1 Technical Specification Reference:

Sections 3.2.1 and 3.4.1.

1.2 <u>Description:</u>

Tables 1-1 and 1-2 are used to determine the maximum average planar linear heat generation rate (MAPLHGR) limit for each fuel type. Limits listed in Tables 1-1 and 1-2 are for Dual Reactor Recirculation Loop Operation.

For Single Reactor Recirculation Loop Operation (SLO), the MAPLHGR limits given in Tables 1-1 and 1-2 must be multiplied by a SLO MAPLHGR multiplier. The SLO MAPLHGR multiplier for SPC fuel is 0.84 (Reference 3 Section 16). The SLO MAPLHGR multiplier for GE14 fuel is 0.77 (Reference 3 Section 16).

Table 1-1

Maximum Average Planar Linear Heat

Generation Rate (MAPLHGR) for SPC ATRIUM-9B Fuel ATRM9-P9DATB326-11GZ-SPC80M-9WR-144-T6-2447 ATRM9-P9DATB326-11GZ-SPC80M-9WR-144-T6-2448 ATRM9-P9DATB339-6GZ-SPC80M-9WR-144-T6-2449 ATRM9-P9DATB362-12GZ-SPC100T-9WR-144-T6-2450 ATRM9-P9DATB360-12GZ-SPC100T-9WR-144-T6-2451 ATRM9-P9DATB378-13GZ-SPC100T-9WR-144-T6-2464 ATRM9-P9DATB378-11GZ-SPC100T-9WR-144-T6-2465 (Bundles2447, 2448, 2449, 2450, 2451, 2464, 2465, bundle types 16, 17, 18, 19, 20, 1 and 2)

(Reference 3 Section 16 and Reference 13)

Planar Average Exposure (GWd/MTU)	MAPLHGR (kW/ft)
0.00	13.52
17.25	13.52
70.00	7.84

Table 1-2

Maximum Average Planar Linear Heat

Generation Rate (MAPLHGR) for GE14 Fuel GE14-P10DNAB408-16GZ-100T-145-T6-2554 GE14-P10DNAB411-4G7.0/9G6.0-100T-145-T6-2553 (Bundles 2553 and 2554, bundle types 3 and 4)

(Reference 3 Section 16)

Planar Average Exposure (GWd/MTU)	MAPLHGR (kW/ft)		
0.00	11.68		
16.00	11.68		
55.12	8.01		
63.50	6.97		
70.00	4.36		

2. Minimum Critical Power Ratio

2.1 <u>Technical Specification Reference:</u>

Sections 3.2.2, 3.4.1 and 3.7.7.

2.2 <u>Description:</u>

The various MCPR limits are described below.

2.2.1 Manual Flow Control MCPR Limits

The Operating Limit MCPR (OLMCPR) is determined from either section 2.2.1.1 or 2.2.1.2, whichever is greater at any given power and flow condition.

2.2.1.1 Power-Dependent MCPR

For operation at less than 38.5% core thermal power, the OLMCPR as a function of core thermal power is shown in Table 2-3. For operation at greater than 38.5% core thermal power, the OLMCPR as a function of core thermal power is determined by multiplying the applicable EOOS condition limit shown in Table 2-1 or 2-2 by the applicable MCPR multiplier K_P given in Table 2-3. For operation at exactly 38.5% core thermal power, the OLMCPR as a function of core thermal power is the higher of either of the two aforementioned methods evaluated at exactly 38.5% core thermal power.

2.2.1.2 Flow-Dependent MCPR

Tables 2-4 and 2-5 provide the MCPR_F limit as a function of flow. The MCPR_F limit determined from these tables is the flow dependent OLMCPR.

2.2.2 <u>Automatic Flow Control MCPR Limits</u>

Automatic Flow Control MCPR Limits are not provided.

2.2.3 Option A and Option B

Option A and Option B refer to scram speeds.

Option A scram speed is the Improved Technical Specification scram speed. The core average scram speed insertion time for 20% insertion must be less than or equal to the Technical Specification Scram Speed to utilize Option A MCPR limits. Reload analyses performed by Global Nuclear Fuel (GNF) for cycle 18 Option A MCPR limits utilized a 20% core average insertion time of 0.900 seconds (Reference 7 Page 6).

To utilize the MCPR limits for the Option B scram speed, the core average scram insertion time for 20% insertion must be less than or equal to 0.694 seconds (Reference 7 Page 6). If the core average scram insertion time does not meet the Option B criteria, but is within the Option A criteria, the appropriate MCPR value may be determined from a linear interpolation between the Option A and B limits with standard

mathematical rounding to two decimal places. When performing a linear interpolation to determine MCPR limits, ensure that the time used for Option A is 0.900 seconds, which is the 20% insertion time utilized by GNF in the reload analysis.

2.2.4 Recirculation Pump Motor Generator Settings

Cycle 18 was analyzed with a maximum core flow runout of 110%; therefore the Recirculation Pump Motor Generator scoop tube mechanical and electrical stops must be set to maintain core flow less than 110% (107.8 Mlb/hr) for all runout events (Reference 12 Section 15). This value is consistent with the analyses of Reference 5.

Table 2-1
MCPR Option A Based Operating Limits
(Reference 3 Appendix G and Reference 14)

		Cycle Exposure			
EOOS Combination	Fuel Type	<13,800 MWd/MT	≥13,800 MWd/MT		
Base Case	GE14	1.53	1.65		
base Case	ATRIUM-9B	1.52	1.61		
Base Case SLO	GE14	1.54	1.66		
Dase Case SLO	ATRIUM-9B	1.53	1.62		
TBPOOS	GE14	1.73	1.75		
166003	ATRIUM-9B	1.67	1.69		
TRROOS SLO	GE14	1.74	1.76		
TBPOOS SLO	ATRIUM-9B	1.68	1.70		
TCV Slow Closure	GE14	1.63	1.65		
TCV Slow Closure	ATRIUM-9B	1.58	1.61		
TOV Class Classes CLO	GE14	1.64	1.66		
TCV Slow Closure SLO	ATRIUM-9B	1.59	1.62		
PLUOOS	GE14	1.68	1.68		
PL0005	ATRIUM-9B	1.63	1.63		
BLUGGE CLO	GE14	1.69	1.69		
PLUOOS SLO	ATRIUM-9B	1.64	1.64		
TOV Church Closed	GE14	1.53	1.65		
TCV Stuck Closed	ATRIUM-9B	1.52	1.61		
TOV Obriel Olese d Cl O	GE14	1.54	1.66		
TCV Stuck Closed SLO .	ATRIUM-9B	1.53	1.62		

Table 2-2
MCPR Option B Based Operating Limits
(Reference 3 Appendix G, Reference 14 and Reference 9 page 9)

		Cycle Exposure			
EOOS Combination	Fuel Type	<13,800 MWd/MT	≥13,800 MWd/MT		
Base Case	GE14	1.42	1.48		
base Case	ATRIUM-9B	1.41	1.44		
Base Case SLO	GE14	1.43	1.49		
base case SLO	ATRIUM-9B	1.42	1.45		
TBPOOS	GE14	1.56	1.58		
16005	ATRIUM-9B	1.50	1.52		
TRROOS SLO	GE14	1.57	1.59		
TBPOOS SLO	ATRIUM-9B	1.51	1.53		
TCV Slow Closure	GE14	1.46	1.48		
1CV Slow Closure	ATRIUM-9B	1.41	1.44		
TCV Class Classes CLO	GE14	1.47	1.49		
TCV Slow Closure SLO	ATRIUM-9B	1.42	1.45		
PLUOOS	GE14	1.51	1.51		
PLUUUS	ATRIUM-9B	1.46	1.46		
BLUOOS SLO	GE14	1.52	1.52		
PLUOOS SLO	ATRIUM-9B	1.47	1.47		
TOV Church Classed	GE14	1.43	1.48		
TCV Stuck Closed	ATRIUM-9B	1.43	1.44		
TOV Chiefs Classed Cl C	GE14	1.44	1.49		
TCV Stuck Closed SLO	ATRIUM-9B	1.44	1.45		

Table 2-3 MCPR_P for GE and SPC Fuel

(Reference 3 Appendix G)

						Core Thermal Power (% of rated)					
EOOS Combination	Core Flow	0	25	38.5	38.5	45	60	70	70	100	
	(% of rated)	Oper	rating Limit N	ACPR .	Operating Limit MCPR Multiplier, K _P						
Pose Cose	≤ 60	3.16	2.58	2.27	1.32	32 1.28	1.15		4.00	1.00	
Base Case	> 60	3.77	2.99	2.56	1.32	1.20	1,10			1.00	
Base Case SLO	≤ 60	3.17	2.59	2.28	1.32	1.28	1.15	A CONTRACT OF		1.00	
Dase Case SLO	> 60	3.78	3.00	2.57	1.32		1.10			1.00	
TRROOS	≤ 60	5.55	3.77	2.82	1.37	1.28	1.15			1.00	
TBPOOS	> 60	6.79	4.62	3.45	1.37					1.00	
TBPOOS SLO	≤ 60	5.56	3.78	2.83	1.37	1.28	1.15	100 mg		1.00	
TBPOOS SLO	> 60	6.80	4.63	3.46						1.00	
TCV Slow Closure	≤ 60	5.55	3.77	2.82	1.64		1.45	1.26	1.11	1.00	
TOV Slow Closule	> 60	6.79	4.62	3.45							
TCV Slow Closure SLO	≤ 60	5.56	3.78	2.83	1.64		1.45	1.26	1.11	1.00	
1 CV Slow Closule SLO	> 60	6.80	4.63	3.46			1.20	1.11	1.00		
PLUOOS	≤ 60	5 55	3.77	2 82	1.64		1.45	1.26	1.11	1.00	
PL0003	> 60	6.79	4.62	3.45	1.04		1,40	1.20	1,11	1.00	
PLUOOS SLO	≤ 60	5.56	3.78	2.83	4.64	1.64		1.45	1.26	1.11	1.00
PE0003 3E0	> 60	6 80	4 63	3.46	1.04		1.45	1.20	1.11	1.00	
TCV Stuck Closed	≤ 60	3.16	2.58	2.27	122 129	1.28	1 15			1.00	
TOV Stuck Closed	> 60	3.77	2.99	2.56	1.32	1.20	1.15			1.00	
TOV Shork Classed SLO	≤ 60	3.17	2.59	2.28	1 22	4 20	4.00		7	4.00	
TCV Stuck Closed SLO	> 60	3.78	3.00	2.57	1.32	1 28	1.15		100	1.00	

Notes for Table 2-3:

- Values are interpolated between relevant power levels.
- For thermal limit monitoring at greater than 100% core thermal power, the 100% core thermal power multiplier, K_P, should be applied.
- Allowable EOOS conditions are listed in Section 5.
- MCRP_P limits are independent of scram speed.

Table 2-4

MCPR_F limits for all fuel types and all operating conditions except TCV Stuck Closed (Reference 9 Page 8)

Flow (% rated)	MCPR _F
110.0	1.22
100.0	1.22
0.0	1.86

Notes for Tables 2-4:

- Values are interpolated between relevant flow values.
- Rated flow is 98 Mlb/hr.
- MCRP_F limit is independent of scram speed.
- This table is not applicable to TCV Stuck Closed operating conditions.

Table 2-5
MCPR_F limits for all fuel types with a TCV Stuck Closed
(Reference 9 Page 8)

Flow (% rated)	MCPR _F
110.0	1.27
108.9	1.27
0.0	1.97

Notes for Tables 2-5:

- Values are interpolated between relevant flow values.
- Rated flow is 98 Mlb/hr.
- MCRP_F limit is independent of scram speed.
- This table is only applicable to TCV Stuck Closed operating conditions.

3. **Linear Heat Generation Rate**

3.1 **Technical Specification Reference:**

Section 3.2.3.

3.2 Description:

The linear heat generation rate (LHGR) limit is the product of the LHGR Limit from Tables 3-1, 3-2, or 3-3 and the minimum of either the power dependent LHGR Factor, LHGRFACP, or the flow dependent LHGR Factor, LHGRFAC_F. The applicable power dependent LHGR Factor (LHGRFAC_P) is determined from Table 3-4. The applicable flow dependent LHGR Factor (LHGRFAC_F) is determined from Tables 3-5 and 3-6.

Table 3-1 LHGR Limits for Bundle Types GE14-P10DNAB408-16GZ-100T-145-T6-2554 (Bundle 2554, bundle type 4)

(Reference 4 Page 6				
dal Exposi	ure	LH		
(CIA/A/AIT)				

Nodal Exposure (GWd/MT)	LHGR Limit (kW/ft)
0.00	13.20
10.00	13.20
13.22	12.90
14.33	12.45
18.73	11.74
27.50	10.40
55.11	7.70
63.61	4.48

Table 3-2 **LHGR Limits for Bundle Types** GE14-P10DNAB411-4G7.0/9G6.0-100T-145-T6-2553 (Bundle 2553, bundle type 3)

(Reference 4 Page 6)

Nodal Exposure (GWd/MT)	LHGR Limit (kW/ft)
0.00	13.40
12.50	13.40
14.33	12.90
22.04	11.90
44.09	9.00
55.00	7.95
58.10	7.20
63.02	5.00

Table 3-3

LHGR Limits for SPC ATRIUM-9B Fuel
ATRM9-P9DATB326-11GZ-SPC80M-9WR-144-T6-2447
ATRM9-P9DATB326-11GZ-SPC80M-9WR-144-T6-2448
ATRM9-P9DATB339-6GZ-SPC80M-9WR-144-T6-2449
ATRM9-P9DATB362-12GZ-SPC100T-9WR-144-T6-2450
ATRM9-P9DATB360-12GZ-SPC100T-9WR-144-T6-2451
ATRM9-P9DATB378-13GZ-SPC100T-9WR-144-T6-2464
ATRM9-P9DATB378-11GZ-SPC100T-9WR-144-T6-2465
(Bundles 2447, 2448, 2449, 2450, 2451, 2464, 2465, bundle types 16, 17, 18, 19, 20, 1 and 2)

(Reference 8 Figure 2.1)

Nodal Exposure (GWd/MT)	LHGR Limit (kW/ft)		
0.00	14.40		
15.00	14.40		
64.30	7.90		

Table 3-4 LHGRFAC_P for all fuel types

(Reference 3 Appendix G)

EOOS Combination	Core Flow (% of rated)	Core Thermal Power (% of rated)									
		0	25	38.5	38.5	70	70	80	100		
		LHGRFAC _P multiplier									
Base Case	560 050 050 050	0.68			0.86	1.00					
base Case	> 60	0.50	0.56	0.59	0.00	7.5		0.00	1.00		
Base Case SLO	≤ 60	0.50	0.56	0.50	0.68	0.60	702	0.86	1.00		
Dase Case SLO	> 60	0.50	0.56	0.59			Mary Co.	0.86	1.00		
TRROOS	≤ 60	0.22	0.20	0.48	0.54				1.00		
IBPOOS	TBPOOS > 60 0.33 0.39 0.42 0.54	0.54				1.00					
TBPOOS SLO	≤ 60	0.22	0.39	0.48	0.54				1.00		
167003 310	> 60	0.33	0.39	0.42	0.54				1.00		
TCV Slow Closure	≤ 60	0.22	0.39	0.48	0.54	0.73	0.78		1.00		
1 CV Slow Closure	> 60	0.33	0.39	0.42	0.54	0.73			1.00		
TCV Slow Closure SLO	≤ 60	0.22	0.39	0.48	0.54	0.73	0.78		1.00		
1CA 210M CIOSRIE 2FO	> 60	0.33	0.59	0.42		0.54	0.54	0.73	0.76		1.00
DILLOGO	560	0.22	0.48	0.20	0.48	0.54	0.54	0.73	0.78		1.00
PLUOOS	> 60	0.33	0.39	0.42	2 0.54			0.54	0.04 0.73	0.76	
PLUCOS SLO	≤ 60	0.22	0.39	0.48	0.54	0.54	0.70		1.00		
PLUOOS SLO	> 60	0.33		0.42		0.73	0.78		1.00		
TCV Stuck Closed	≤ 60	0.50	0.56	0.59 0.6	0.60			0.06	1.00		
	> 60	0.50			0.08			0.86	1.00		
TCV Stuck Closed SLO	≤ 60	0.50		0.59	0.68			0.00	4.00		
	> 60	0.50 0.56	0.56					0.86	1.00		

Notes for Table 3-4:

- Values are interpolated between relevant power levels.
- For thermal limit monitoring at greater than 100% core thermal power, the 100% core thermal power LHGRFAC_P multiplier should be applied.
- Allowable EOOS conditions are listed in Section 5.
- LHGRFAC_P multiplier is independent of scram speed.

Table 3-5 LHGRFAC_F multipliers

(Reference 5 Figure 3-3)

Flow (% rated)	LHGRFAC _F		
0	0.28		
30	0.55		
40	0.64		
50	0.77		
80	1.00		
100	1.00		
110	1.00		

Table 3-6 LHGRFAC_F multipliers for Turbine Control Valve Stuck Closed

(Reference 5 Table 2-17)

Flow (% rated)	LHGRFAC _F		
0	0.14		
30	0.41		
40	0.50		
50	0.63		
80	0.86		
98.3	1.00		
100	1.00		
110	1.00		

Notes for Tables 3-5 and 3-6:

- Values are interpolated between relevant flow values.
- 98 Mlb/hr is rated flow.
- LHGRFAC_F multipliers are applicable to all fuel types used in cycle 18.
- Table 3-5 is valid for all operating conditions for all EOOS scenarios except TCV stuck closed.
- Table 3-6 is valid for all operating conditions with a TCV stuck closed.
- LHGRFAC_F multipliers are independent of scram speed.

4. Control Rod Withdrawal Block Instrumentation

4.1 <u>Technical Specification Reference:</u>

Table 3.3.2.1-1

4.2 <u>Description:</u>

The Rod Block Monitor Upscale Instrumentation Setpoints are determined from the relationships shown below (Reference 6 Page 11):

ROD BLOCK MONITOR UPSCALE TRIP FUNCTION	ALLOWABLE VALUE
Two Recirculation Loop Operation	0.65 W _d + 55%
Single Recirculation Loop Operation	0.65 W _d + 51%

The setpoint may be lower/higher and will still comply with the Rod Withdrawal Event (RWE) Analysis because RWE is analyzed unblocked.

 W_{d} – percent of drive flow required to produce a rated core flow of 98 Mlb/hr.

5. Allowed Modes of Operation (B 3.2.2, B 3.2.3)

The Allowed Modes of Operation with combinations of Equipment Out-of-Service are as described below:

	OPERATING REGION			
Equipment Out of Service Options ^{1,2,3}	Standard	MELLLA	Coastdown ⁴	
Base Case, Option A or B	Yes	Yes	Yes	
Base Case SLO, Option A or B	Yes	Yes	Yes	
TBPOOS, Option A or B	Yes	Yes	Yes	
TBPOOS SLO, Option A or B	Yes	Yes	Yes	
TCV Slow Closure, Option A or B	Yes	Yes	Yes	
TCV Slow Closure SLO, Option A or B	Yes	Yes	Yes	
PLUOOS, Option A or B	Yes	Yes	Yes	
PLUOOS SLO, Option A or B	Yes	Yes	Yes	
TCV Stuck Closed, Option A or B	Yes	Yes	Yes	
TCV Stuck Closed SLO, Option A or B	Yes	Yes	Yes	

¹ Each OOS Option may be combined with up to 18 TIP channels OOS (provided the requirements for utilizing SUBTIP methodology are met) with all TIPS available at startup from a refuel outage, a 120°F reduction in feedwater temperature throughout the cycle (Final Feedwater Temperature Reduction was analyzed for the entire cycle), and up to 50% of the LPRMs OOS with an LPRM calibration frequency of 2500 Effective Full Power Hours (EFPH) (2000 EFPH +25%).

² Additionally, a single MSIV may be taken OOS (shut) under any and all OOS Options, so long as core thermal power is maintained ≤75% of 2957 MWt (Reference 11).

³ All OOS Options support 1 Turbine Bypass Valve OOS, if the OPL-3 assumed opening profile for the Turbine Bypass system is met. If the OPL-3 opening profile is not met, or if more than one Turbine Bypass Valve is OOS, utilize the TBPOOS condition.

⁴ Coastdown operation is defined as any cycle exposure beyond the full power, all rods out condition with plant power slowly lowering to a lesser value while core flow is held constant (Reference 10 Section 4.3.1.2.8). Up to a 15% overpower is analyzed per Reference 5.

6. Methodology (5.6.5)

The analytical methods used to determine the core operating limits shall be those previously reviewed and approved by the NRC, specifically those described in the following documents:

- 1. ANF-1125 (P)(A) and Supplements 1 and 2, "Critical Power Correlation ANFB," April 1990.
- 2. ANF-524 (P)(A) Revision 2 and Supplements 1 and 2, "ANF Critical Power Methodology for Boiling Water Reactors," November 1990.
- 3. XN-NF-79-71 (P)(A) Revision 2 and Supplements 1, 2 & 3, "Exxon Nuclear Plant Transient Methodology for Boiling Water Reactors," March 1986.
- 4. XN-NF-80-19 (P)(A) Volume 1 Supplements 1 and 2, "Exxon Nuclear Methodology for Boiling Water Reactors Neutronic Methods for Design and Analysis," March 1993.
- 5. XN-NF-80-19 (P)(A) Volume 1 Supplement 3, Supplement 3 Appendix F, and Supplement 4, "Exxon Nuclear Methodology for Boiling Water Reactors," November 1990.
- 6. XN-NF-80-19 (P)(A) Volumes 2, 2A, 2B and 2C, "Exxon Nuclear Methodology for Boiling Water Reactors: EXEM BWR ECCS Evaluation Model," September 1982.
- 7. XN-NF-80-19 (P)(A) Volume 3 Revision 2, "Exxon Nuclear Methodology for Boiling Water Reactors, THERMEX: Thermal Limits Methodology Summary Description," January 1987.
- 8. XN-NF-80-19 (P)(A) Volume 4 Revision 1, "Exxon Nuclear Methodology for Boiling Water Reactors: Application of the ENC Methodology to BWR Reloads," June 1986.
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